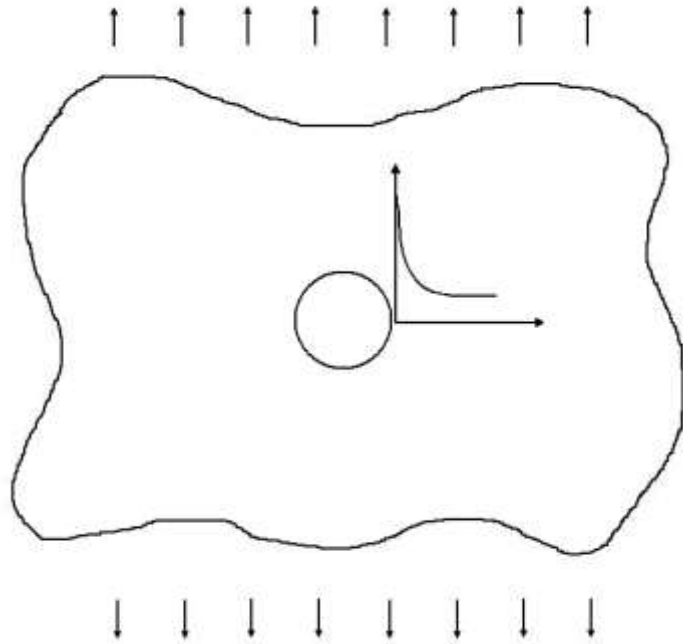


# Stress Intensity Solution Development for Through Cracks at Expanded Holes

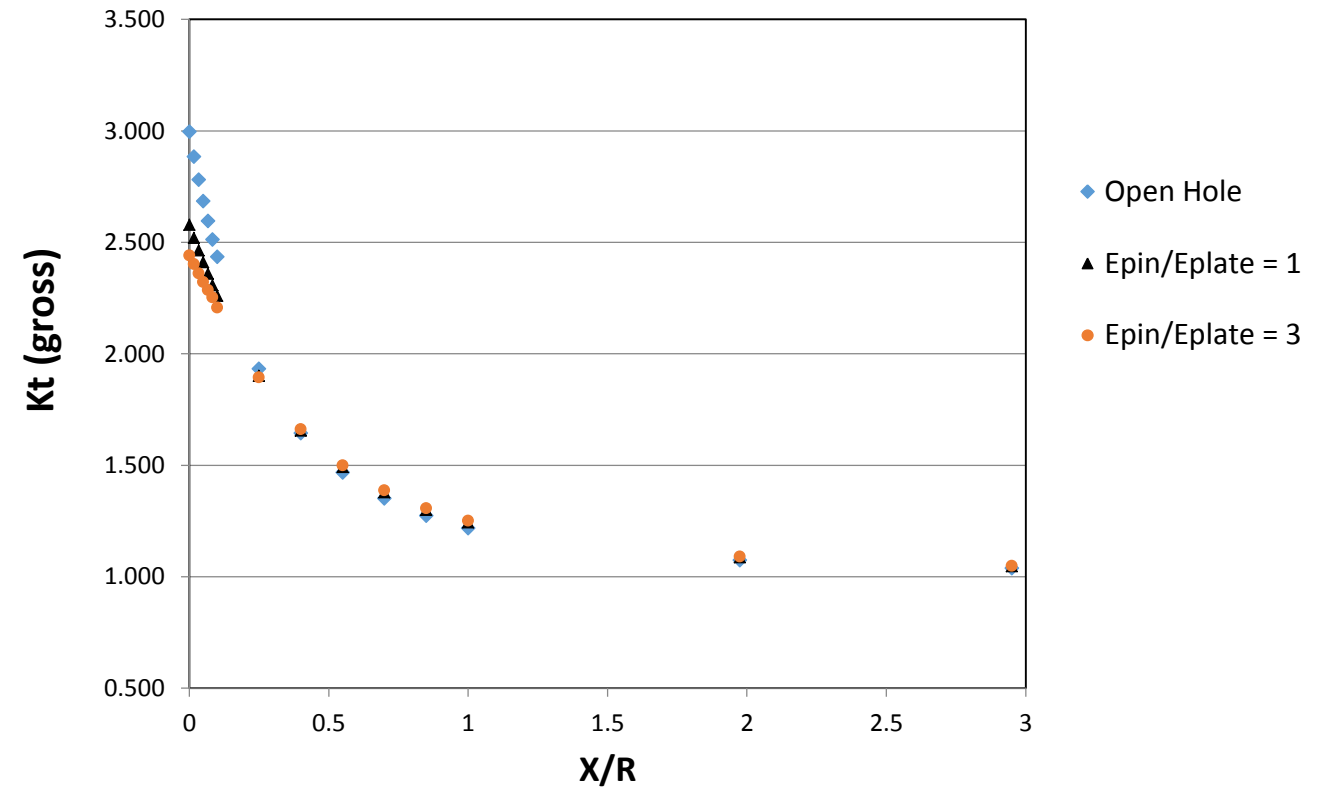
James A. Harter, Consultant  
Cordell E. Smith, LexTech, Inc.

AFGROW Workshop  
Sep 15-16 2015  
Layton, UT

# Stress Distribution from the Edge of a Hole

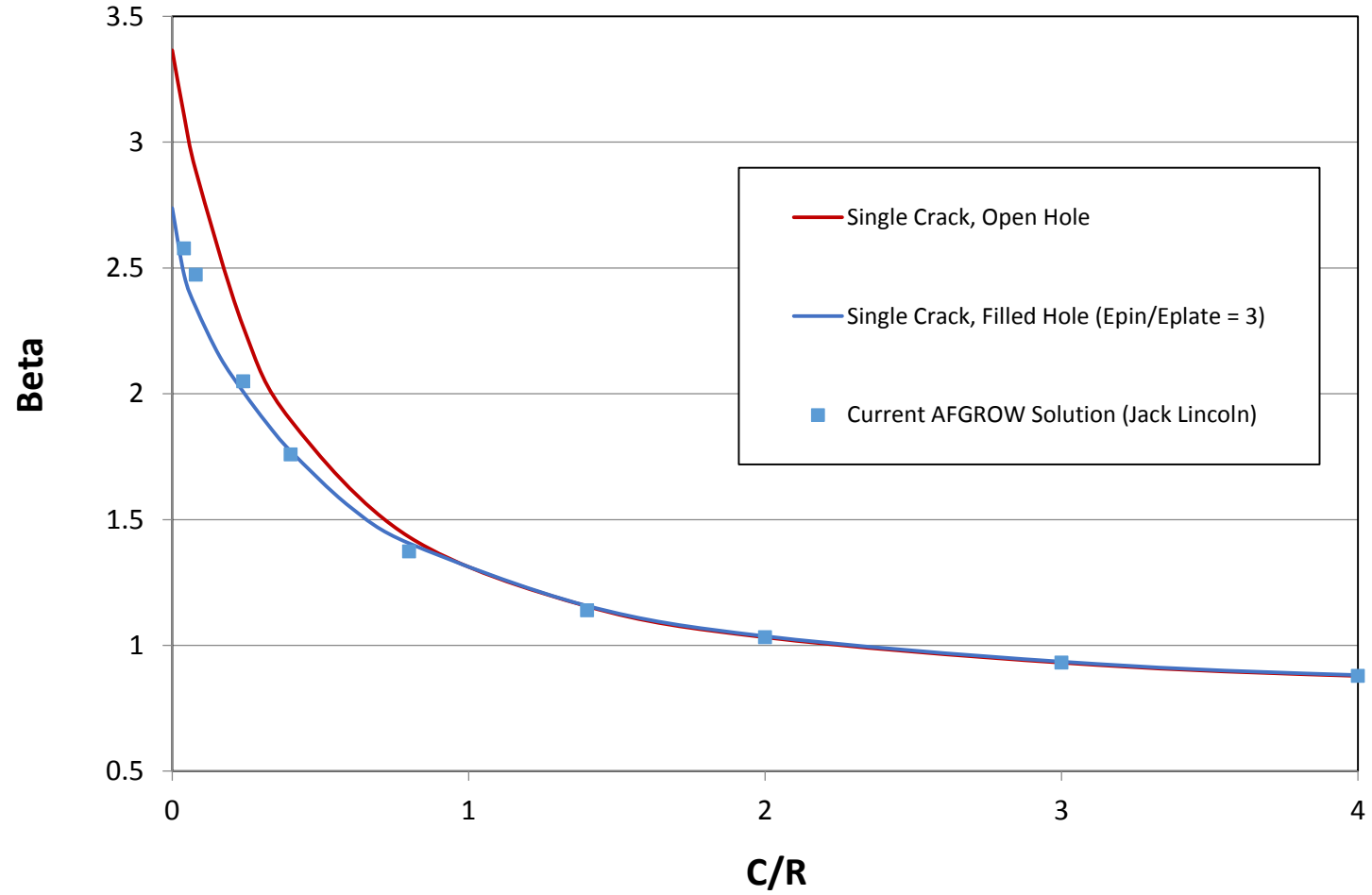


Open vs. Unloaded, Filled Hole  
Uniform Remote Traction



# Single Through Cracked Hole

Infinite Plate, Remote Traction Reference

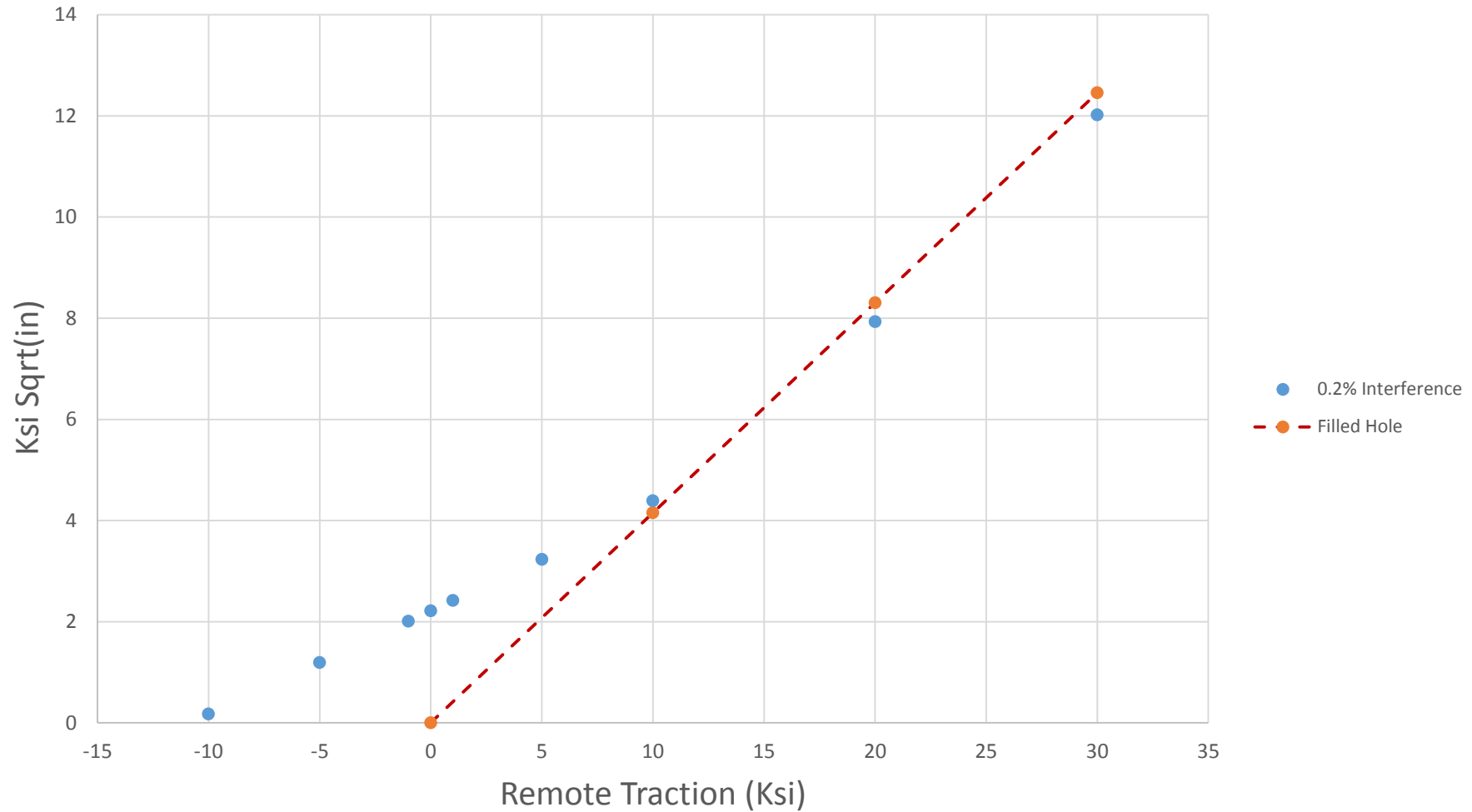


# Effect of Hole Interference

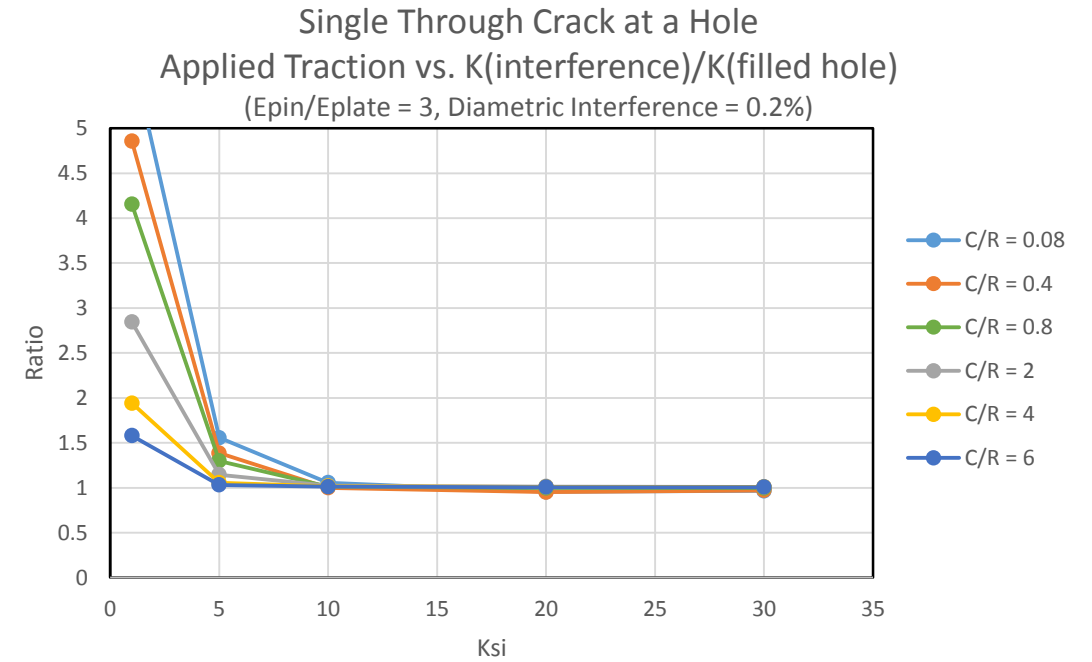
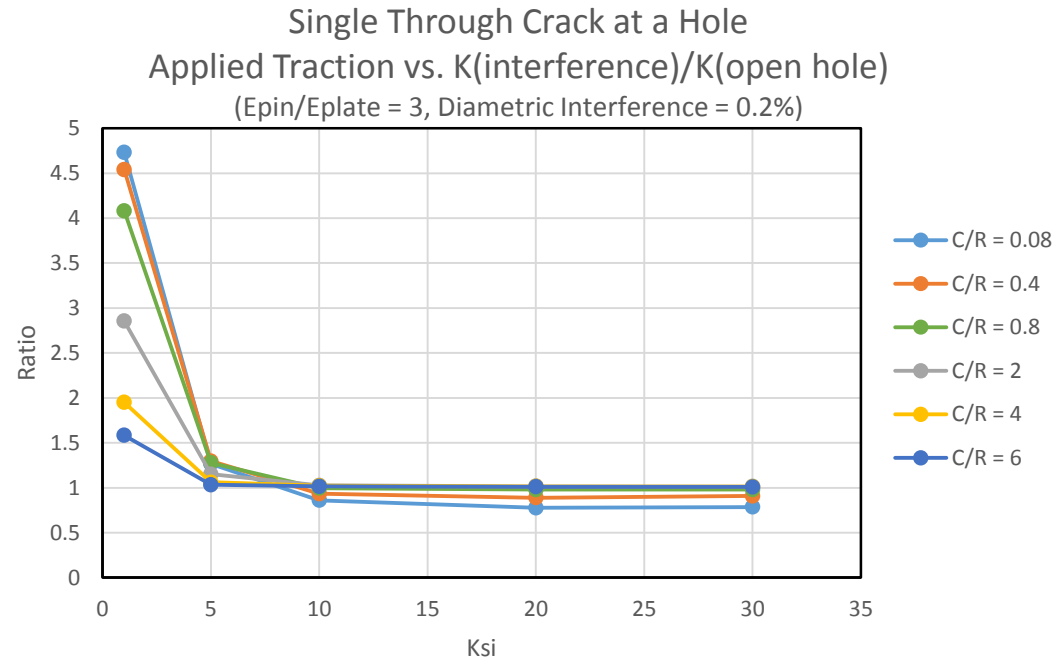
## Applied Traction vs. K

( $E_{pin}/E_{plate} = 3$ , Diametric Interference = 0.2%)

$C/R = 0.08$

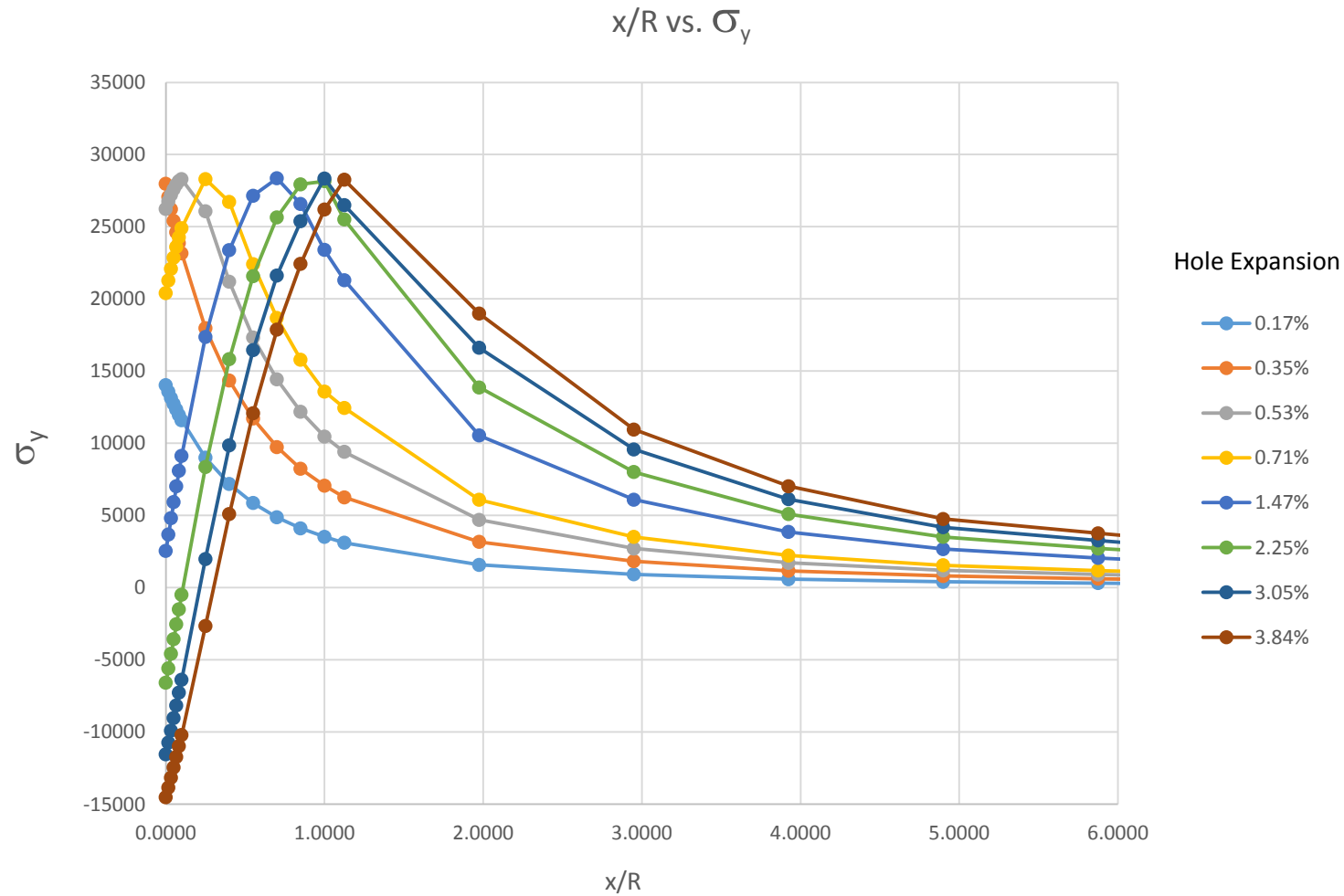


# Using an Open Hole vs. Filled Hole Reference Solution



The expanded hole solution converges to the filled hole solution for all crack lengths

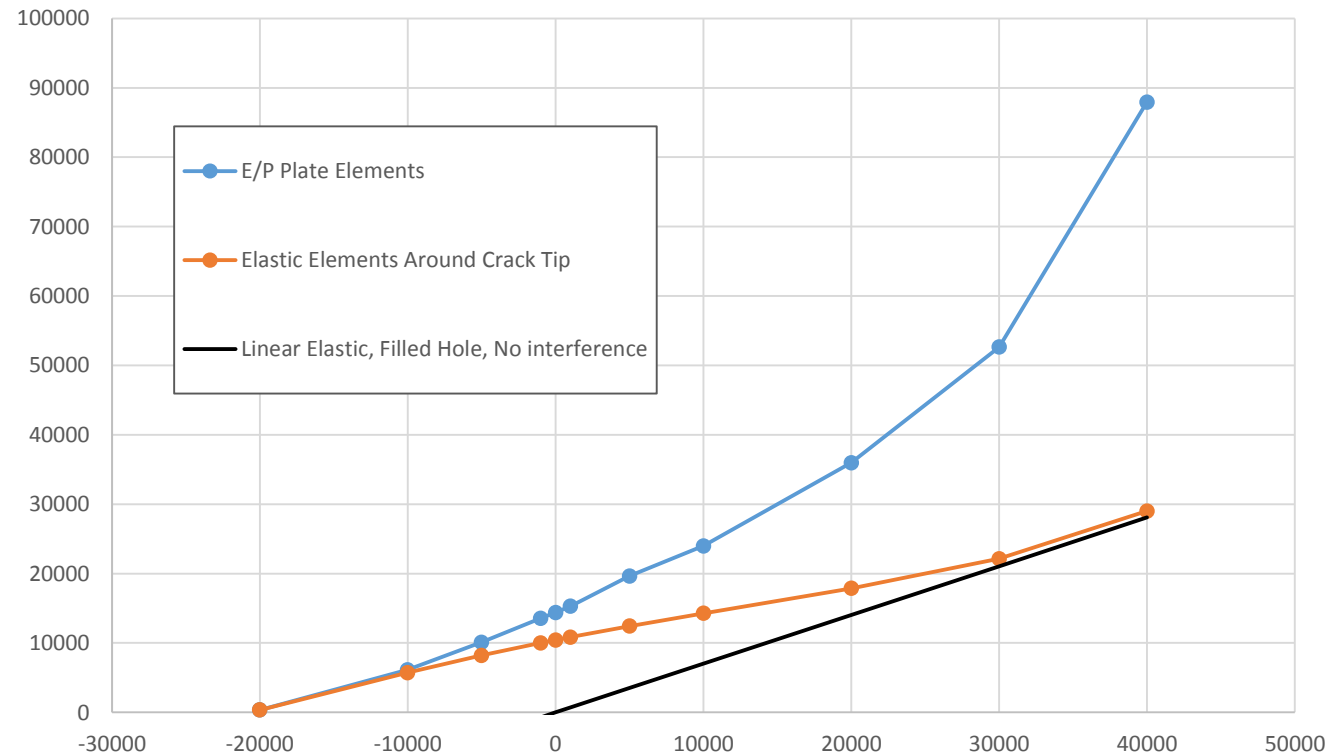
# Un-cracked Model Results



The hole expansion values were determined from  $u_x$  after gen, non-linear iterations. I verified the results were the same for steel and aluminum for the same resulting hole expansion.

# Problem

Applied Remote Traction vs. K  
Single Through Crack (C = 0.05 in., Dia. = 0.25 in.)  
Hole Expansion = 0.001775

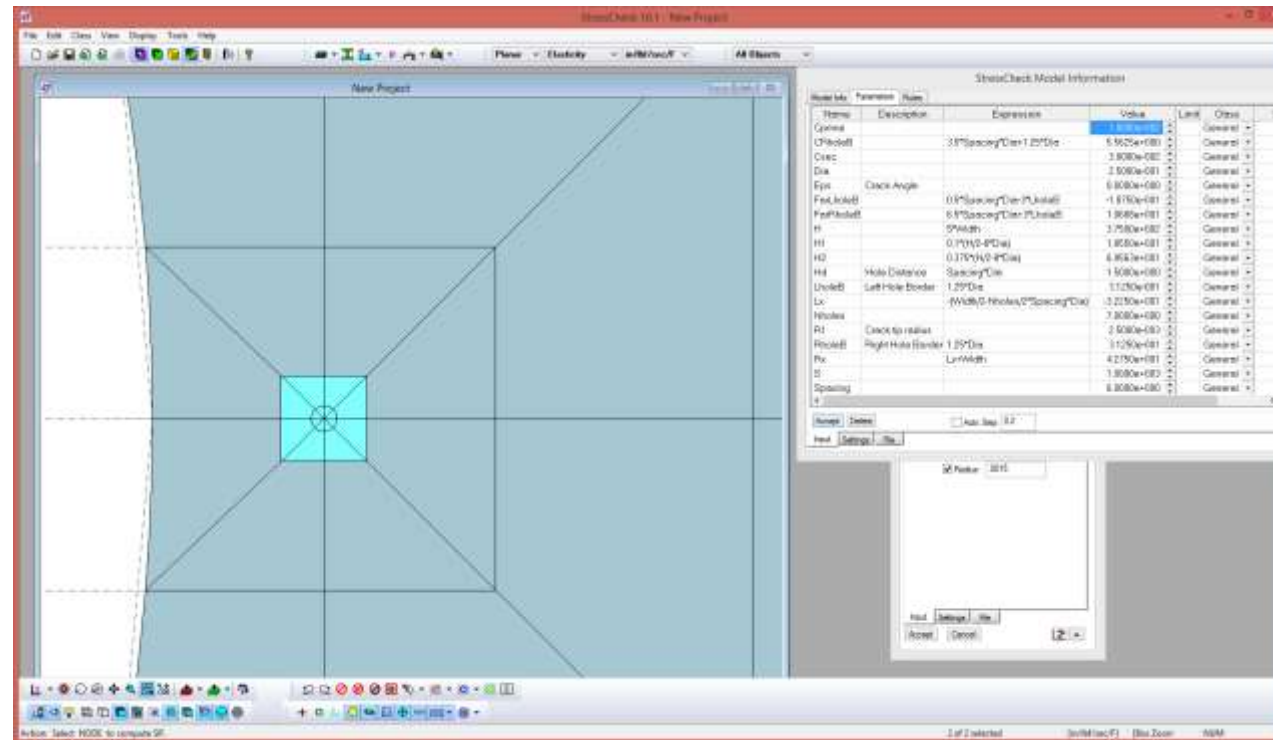


For hole interference cases that are locally plastic, there appeared to be a problem with the resulting stress intensity values shown here for different remote applied tractions. The solutions are diverging. Perhaps this is because the K extraction is ignoring the higher order terms in the J-integral. However, we need to find a way forward.

One idea is to use elastic elements immediately around the crack tip so that the overall effect of the hole expansion is captured, and K extraction is performed in the elastic area at the crack tip. This may help to delay the divergence.

# Hypothesis

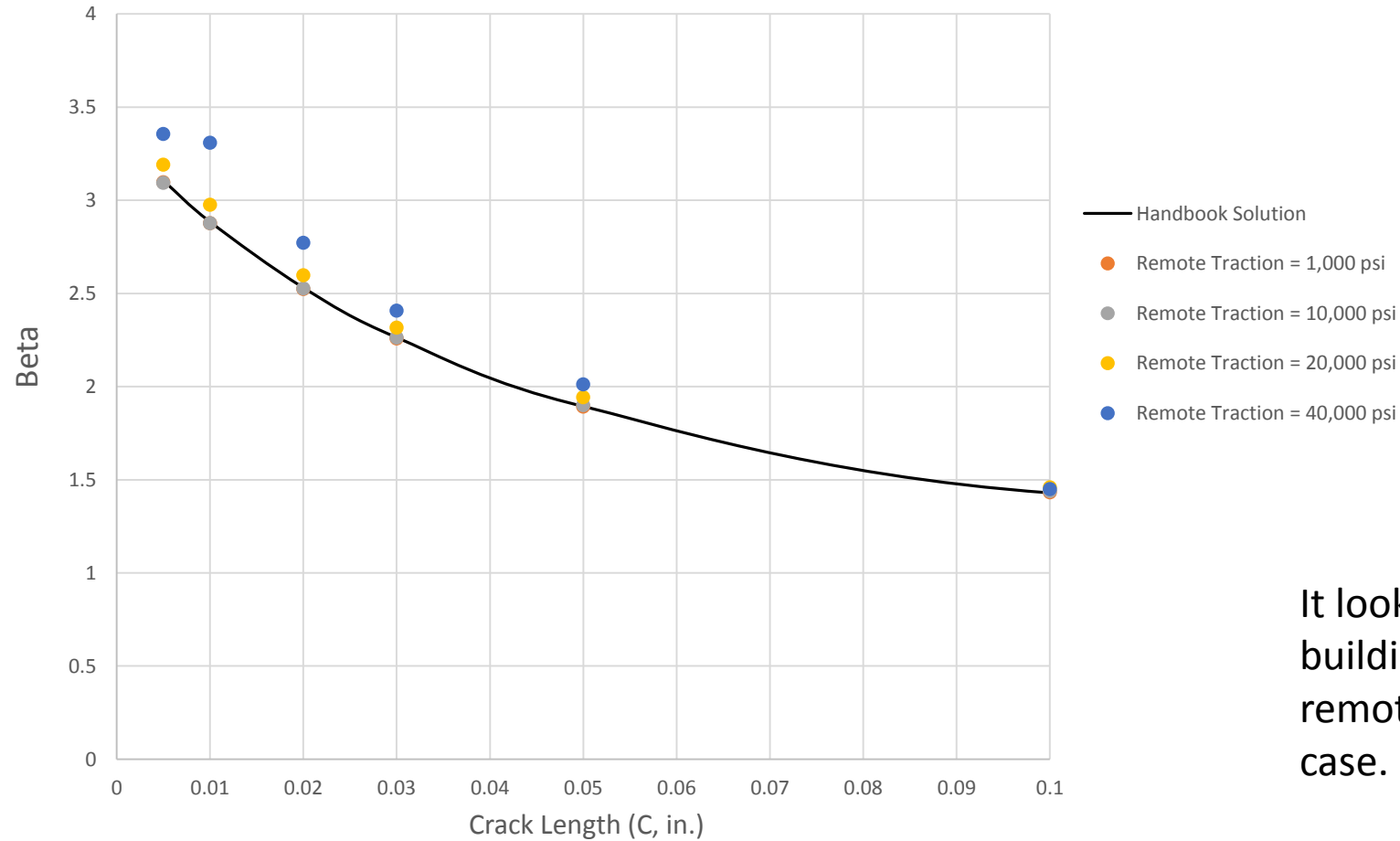
Using elastic elements around the crack tip will result in reasonable K's until the displacement/stress discontinuities at the element boundaries become significant.





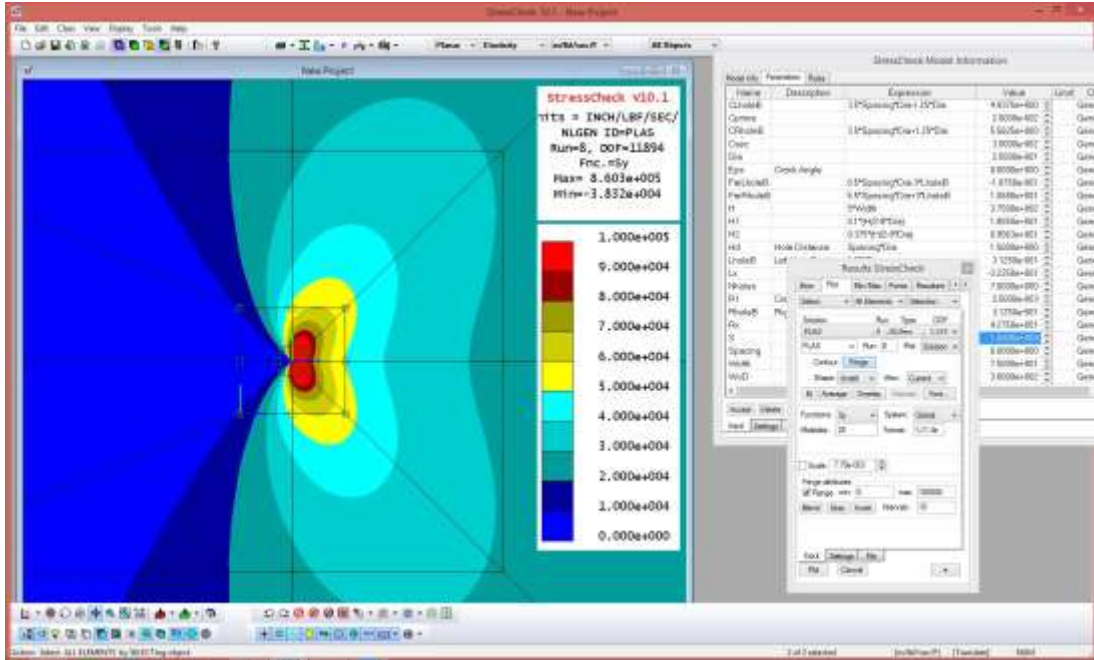
# Verification

Crack Length vs. Beta  
Open Hole, Wide Plate

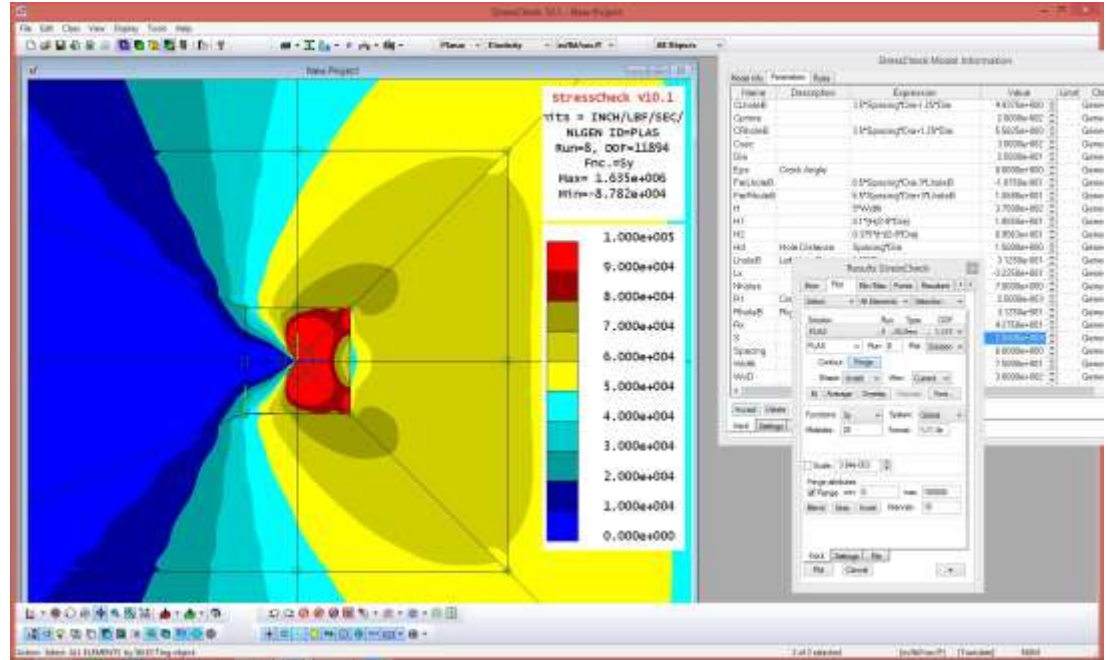


It looks like “Elvis has left the building” at about 20,000 psi applied remote traction for the open hole case.

# Can I Quantify This?



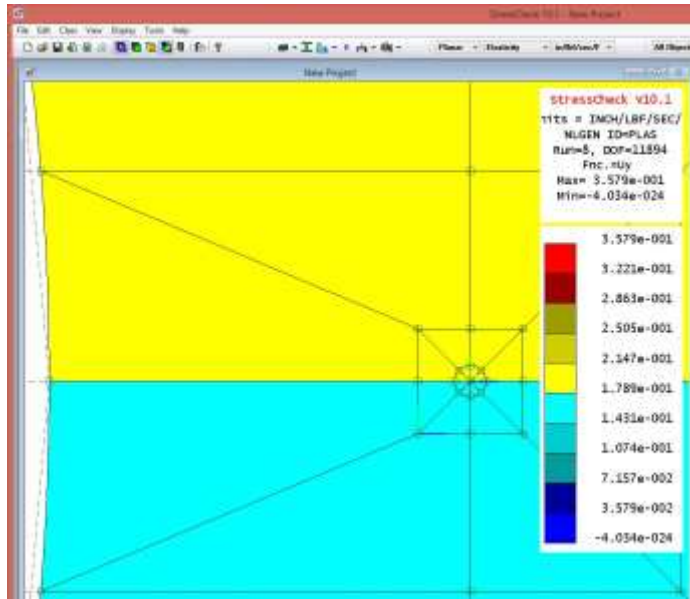
1,000 psi



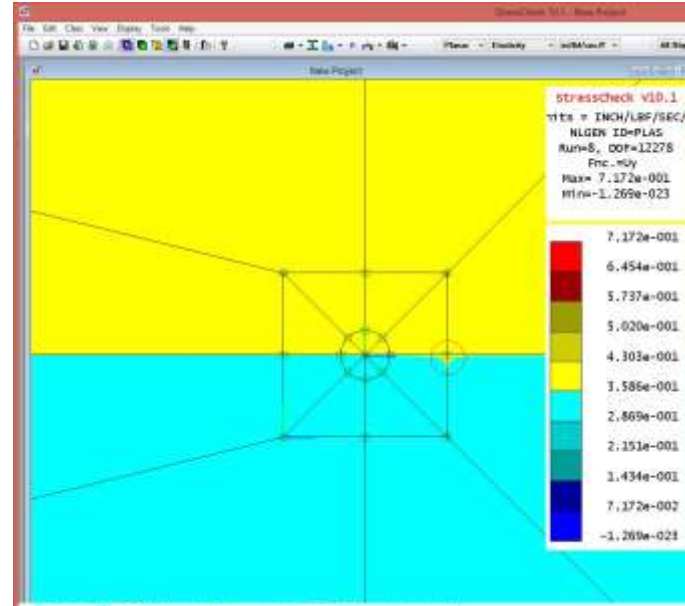
20,000 psi

Now, "Ugly" is generally a relative thing.....

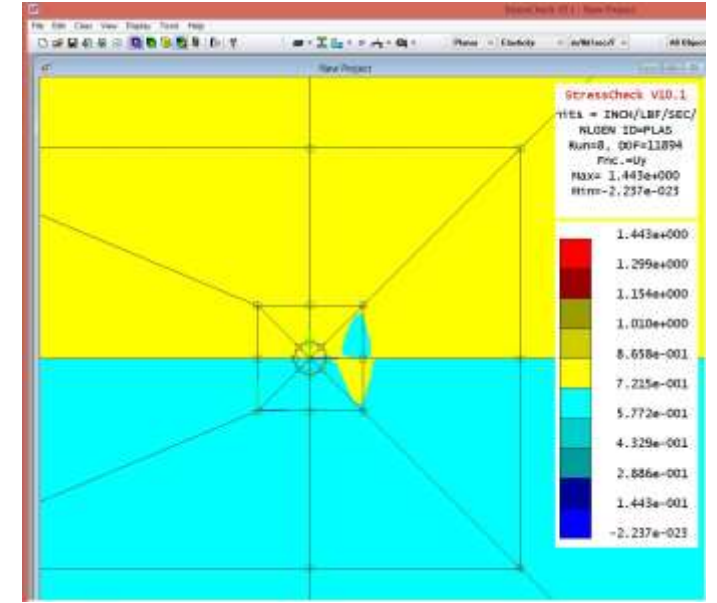
# Now, this looked promising.....



10,000 psi



20,000 psi



40,000 psi

I used the default scaling for  $u_y$  in the fringe plots since StressCheck breaks the fringe at the crack plane. You can see the “bobble” in the  $u_y$  fringe plot is just visible at 20,000 psi (circled on the graphic)

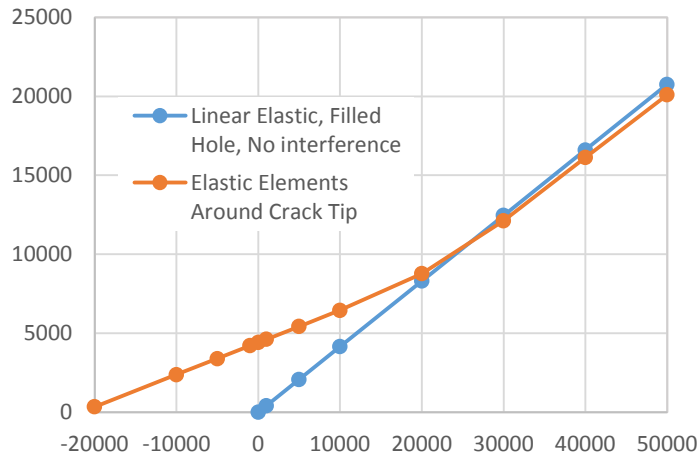
## We Currently Have K-Solutions for:

Interference Levels: 0.4, 0.8, 1.6, 2.4, 3.2, 4.0, & 5.0%

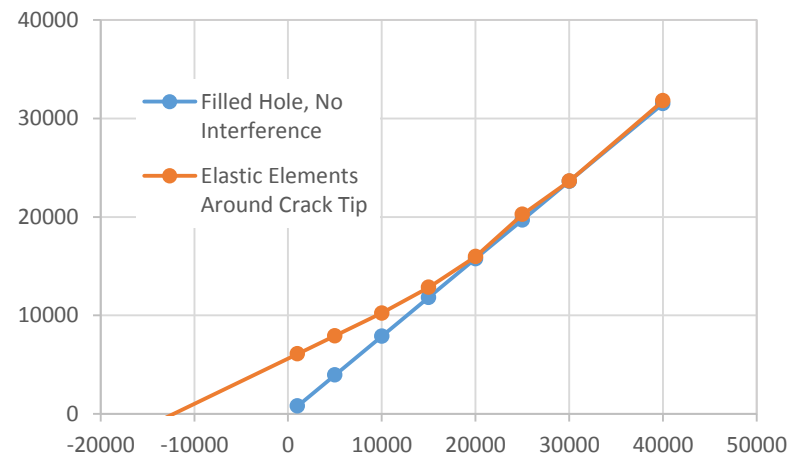
Through Crack Lengths: 0.01 – 0.5 in.

# Low Interference Case (0.4%)

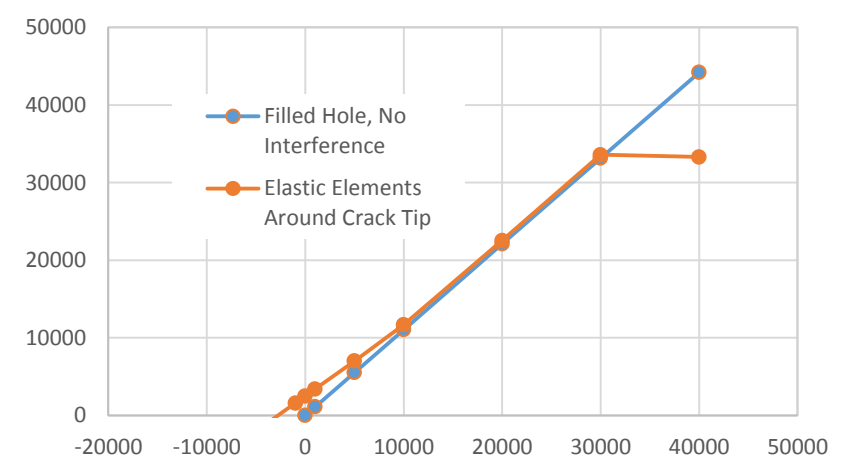
Applied Remote Traction vs. K  
(C=0.01 in, Dia=0.25 in)  
Interference = 0.001



Applied Remote Traction vs. K  
(C=0.1 in, Dia=0.25 in)  
Interference = 0.001

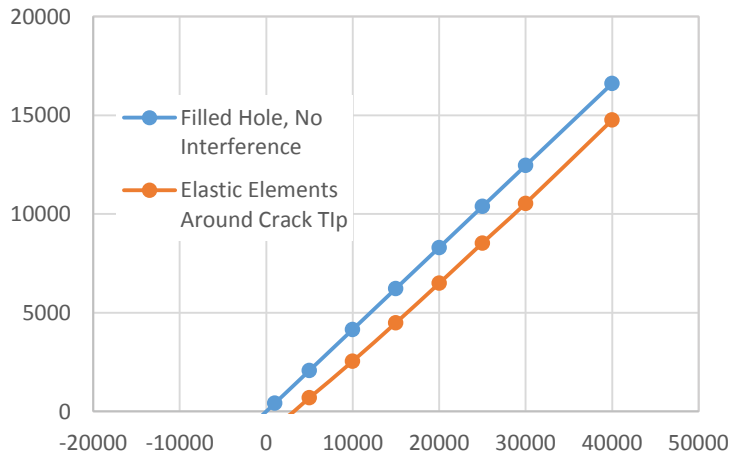


Applied Remote Traction vs. K  
(C=0.5 in, Dia=0.25 in.)  
Interference = 0.001

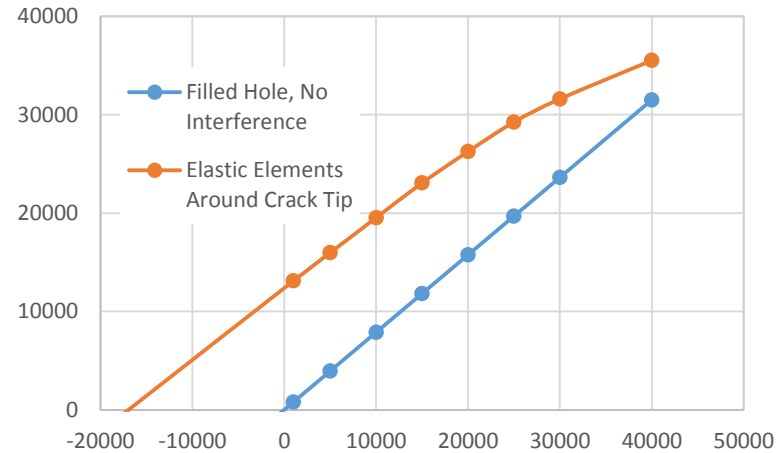


# Moderate Interference Case (2.4%)

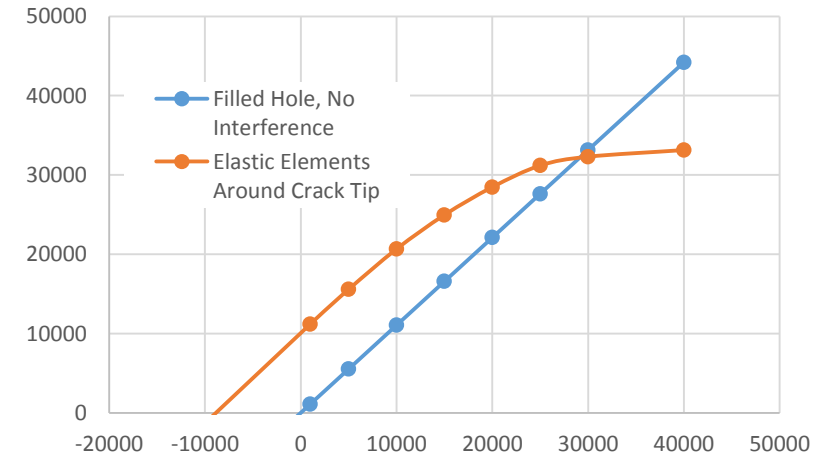
Applied Remote Traction vs. K  
(c=0.01 in., Dia=0.25 in.)  
Interference = 0.006 in.



Applied Remote Traction vs. K  
(c=0.1 in., Dia=0.25 in.)  
Interference = 0.006 in

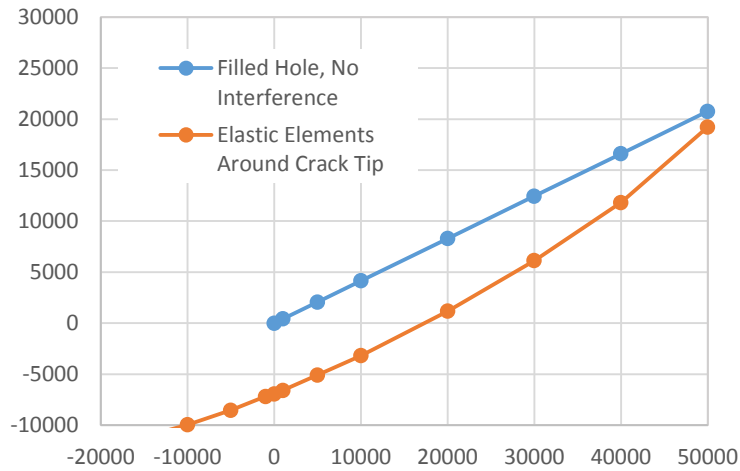


Applied Remote Traction vs. K  
(C=0.5 in., Dia=0.25 in.)  
Interference = 0.006 in.

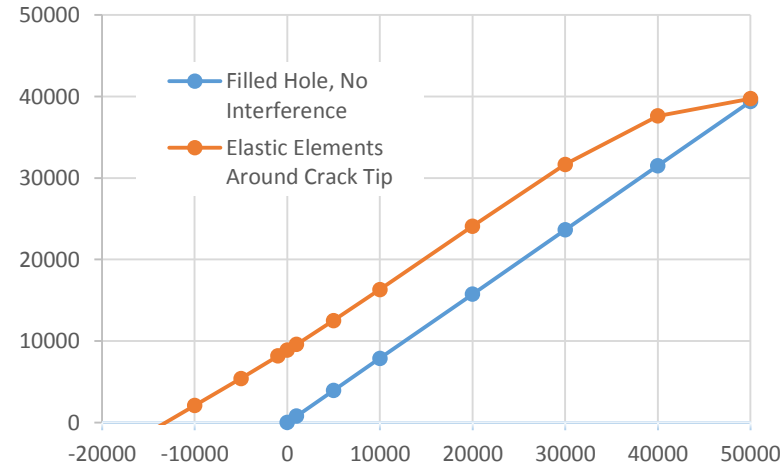


# Moderate Interference Case (4.0%)

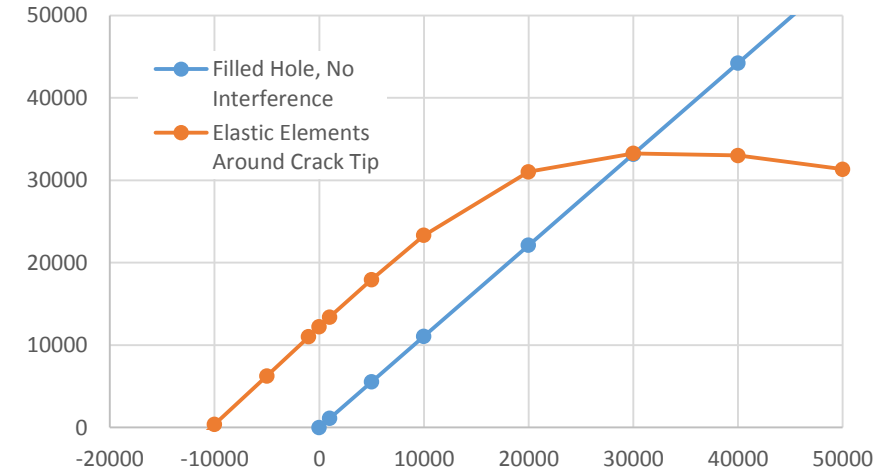
Applied Remote Traction vs. K  
(C=0.01 in., Dia=0.25 in.)  
Interference = 0.01



Applied Remote Traction vs. K  
(C=0.1 in., Dia=0.25 in.)  
Interference = 0.01



Applied Remote Traction vs. K  
(C=0.5 in., Dia=0.25 in.)  
Interference = 0.01



# Discussion

Is this something that should be investigated further so that a solution for cracks at expanded holes can be added to AFGROW?