

Ogden Air Logistics Center



U.S. AIR FORCE

***Comparison of
Advanced Continuing Damage
Model
&
Classic Single Edge Through Crack
Model***

***Tim Allred
A-10 ASIP Group
Hill AFB, UT
801-586-2474***



Acknowledgements



OGDEN AIR LOGISTICS CENTER

- James A. Harter, AFRL/VASM
- Alexander V. Litvinov, LexTech, Inc.
- A-10 ASIP Group



Overview



OGDEN AIR LOGISTICS CENTER

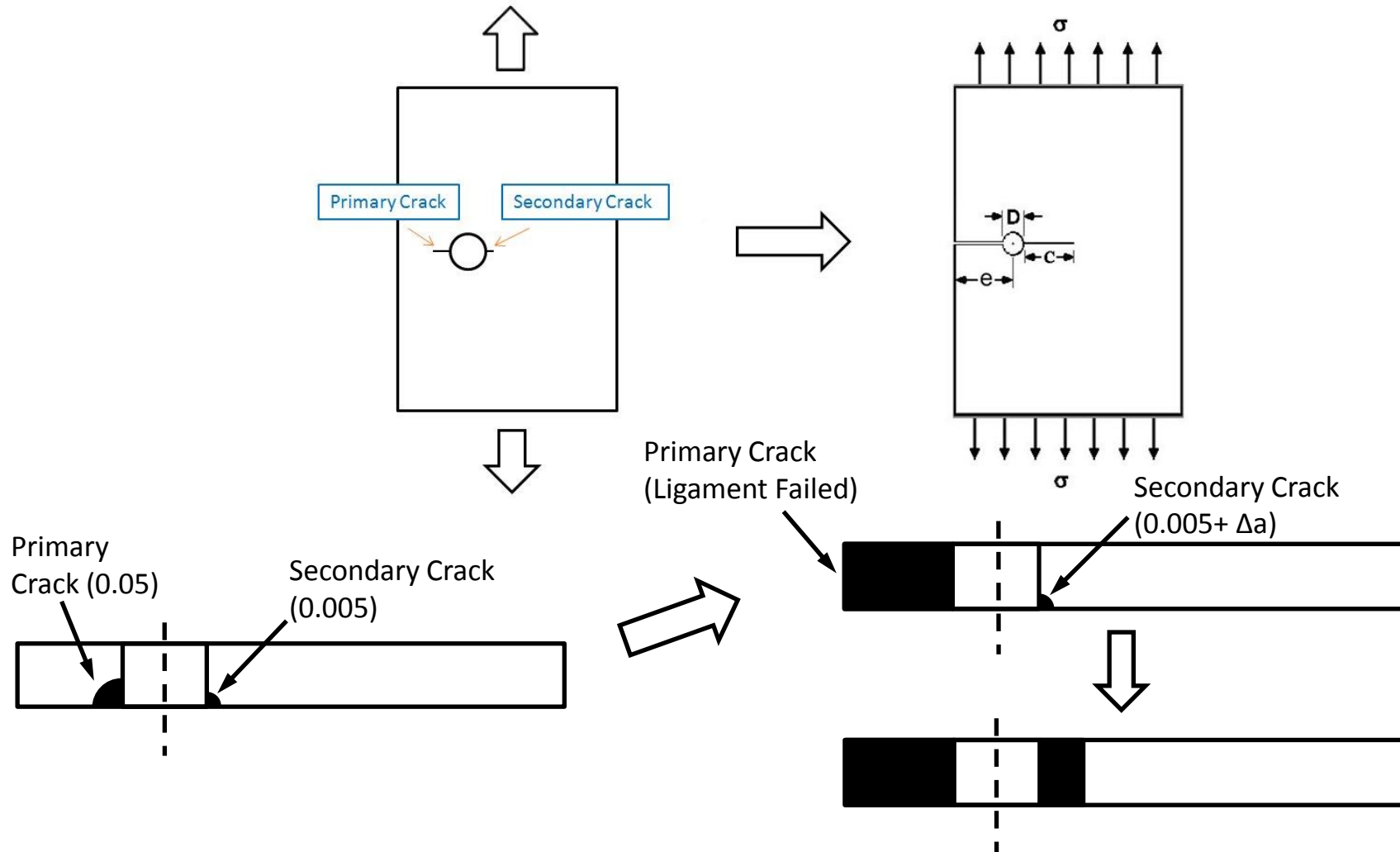
- AFGROW Models
 - Advanced Continuing Damage Model
 - Classic Single Edge Through Crack
- In Plane Bending
- K Solution Comparisons
- FEM Constraints
- Conclusions and Recommendations



Continuing Damage



OGDEN AIR LOGISTICS CENTER



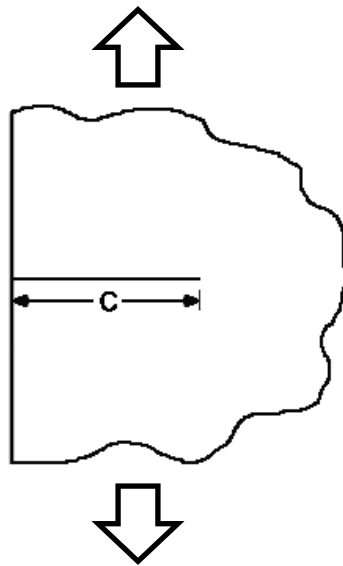


Equivalent Edge Crack Solution



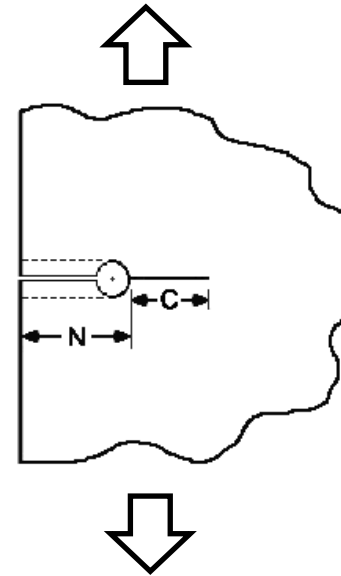
OGDEN AIR LOGISTICS CENTER

Solution for Continuing Damage Model converges with
Edge Crack Solution when $C \geq$ Hole Radius
(Semi-Infinite Plate)



$$K = \sigma \sqrt{\pi C} \beta$$

$$\beta = 1.1221$$



$$\sigma \sqrt{\pi (C + N)} (1.1221) = \sigma \sqrt{\pi C} \beta$$

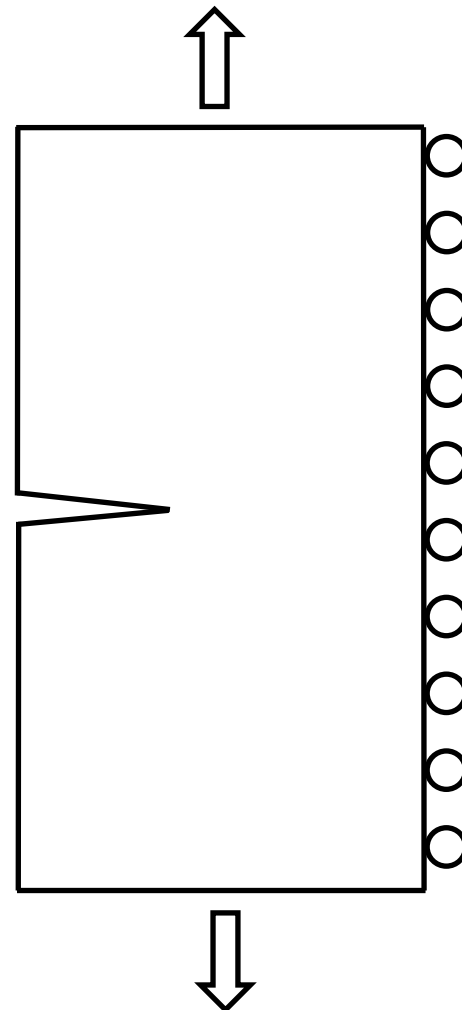
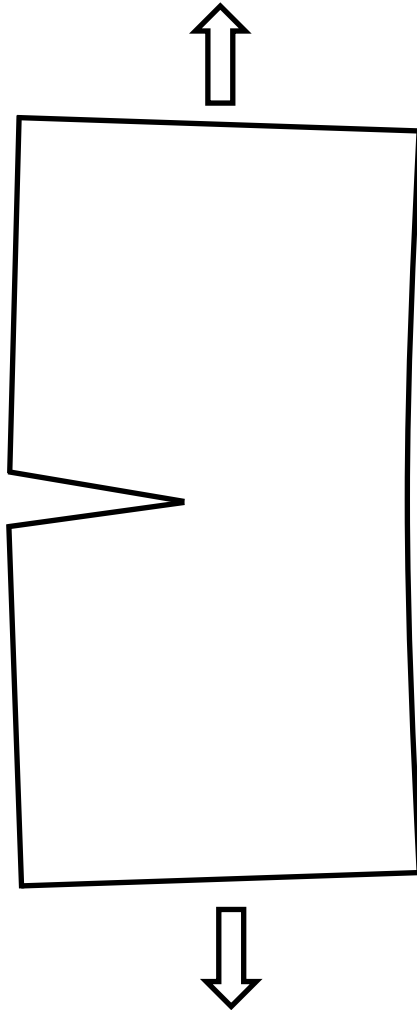
$$\beta = \frac{1.1221}{\sqrt{C/(C + N)}}$$



Finite Width Plates In Plane Bending



OGDEN AIR LOGISTICS CENTER



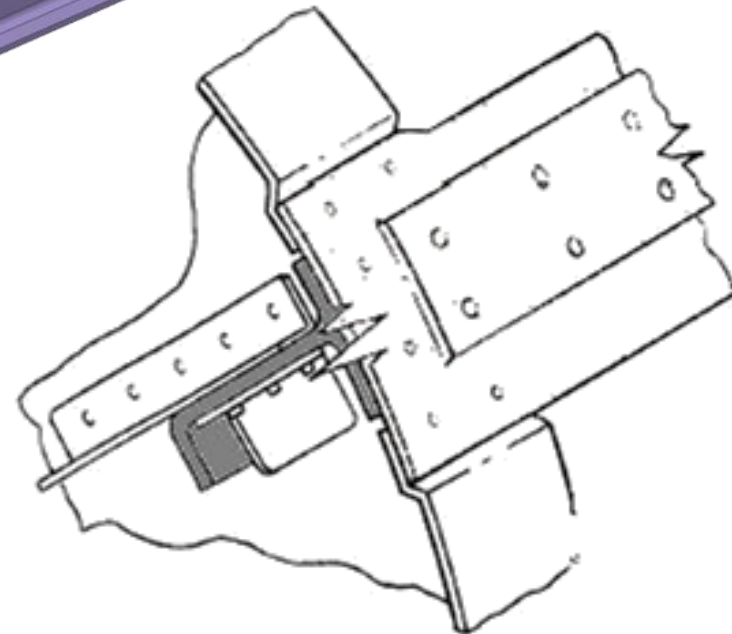
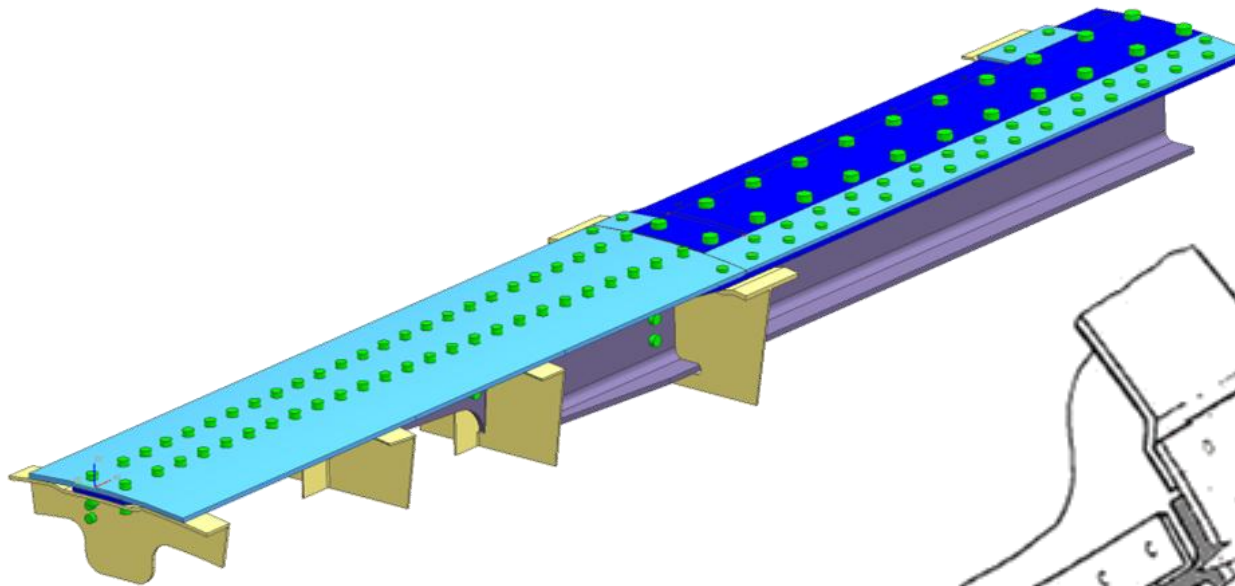


In Plane Bending Constraint



OGDEN AIR LOGISTICS CENTER

Built Up Structure on Aircraft





Stress Intensity Solutions



OGDEN AIR LOGISTICS CENTER

| Model | In Plane Bending Constrained ? | Solution Source | Ref |
|-----------------------------------|--------------------------------|----------------------------|--------------------|
| Advanced Continuing Damage | X | FEM (ABAQUS w/ FRANC3D/NG) | Harter |
| Classic Single Edge Through Crack | X | FEM (FRANC2D) | Taluk |
| Advanced Continuing Damage | | FEM (ABAQUS w/ FRANC3D/NG) | Harter |
| Classic Single Edge Through Crack | | ?? | Tada, Paris, Irwin |

References:

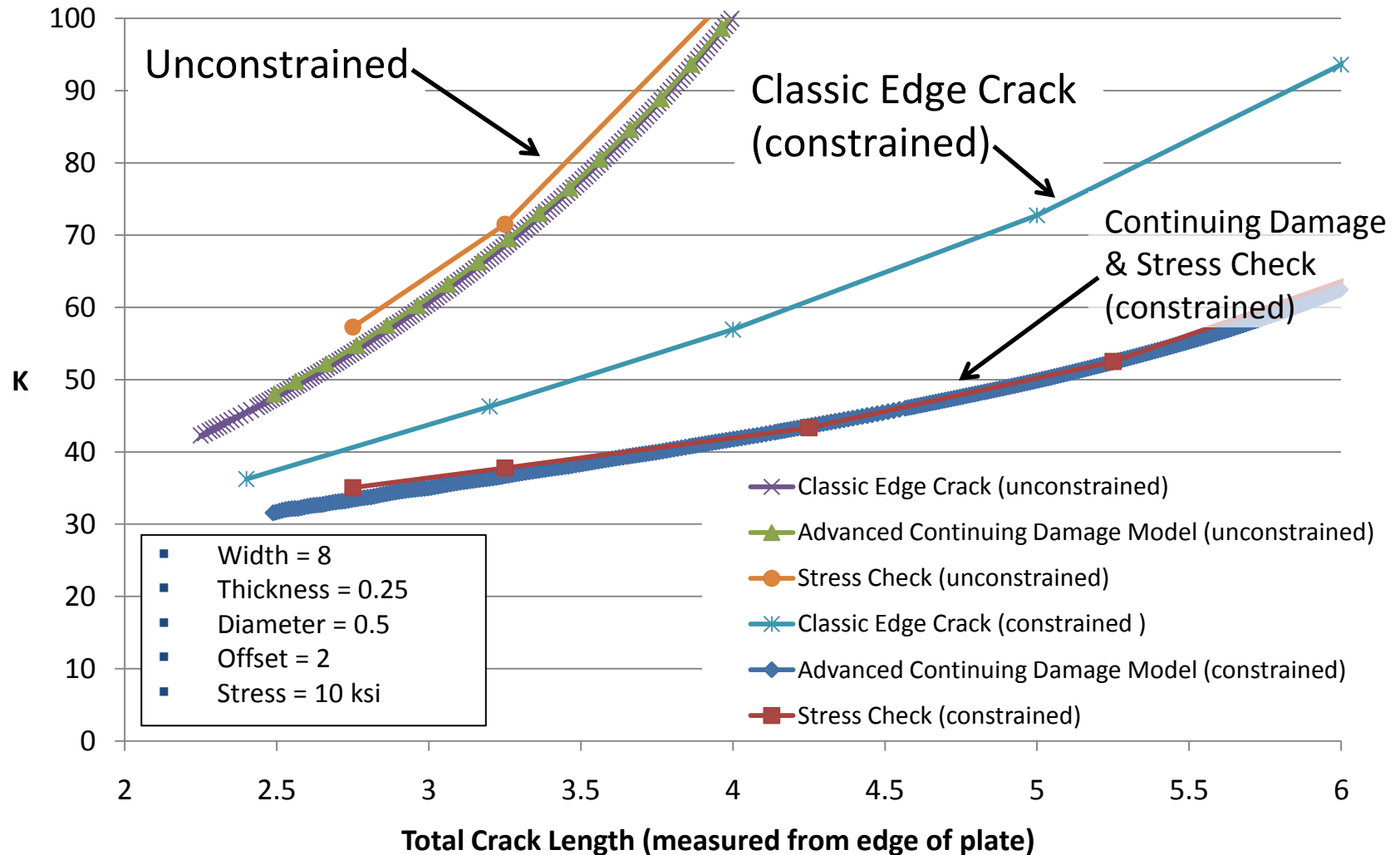
- Harter, James A, AFRL/VASM, 2009
- Taluk, Deviprasad, Eagle Aeronautics, Inc., 1998
- Tada, H., Paris, P.C., and Irwin, G.R., "The Stress Analysis of Cracks Handbook," Second Edition, p. 2.11, Paris Productions, Inc., St Louis, MO, 1985



AFGROW Finite Width Plate K Solutions



OGDEN AIR LOGISTICS CENTER

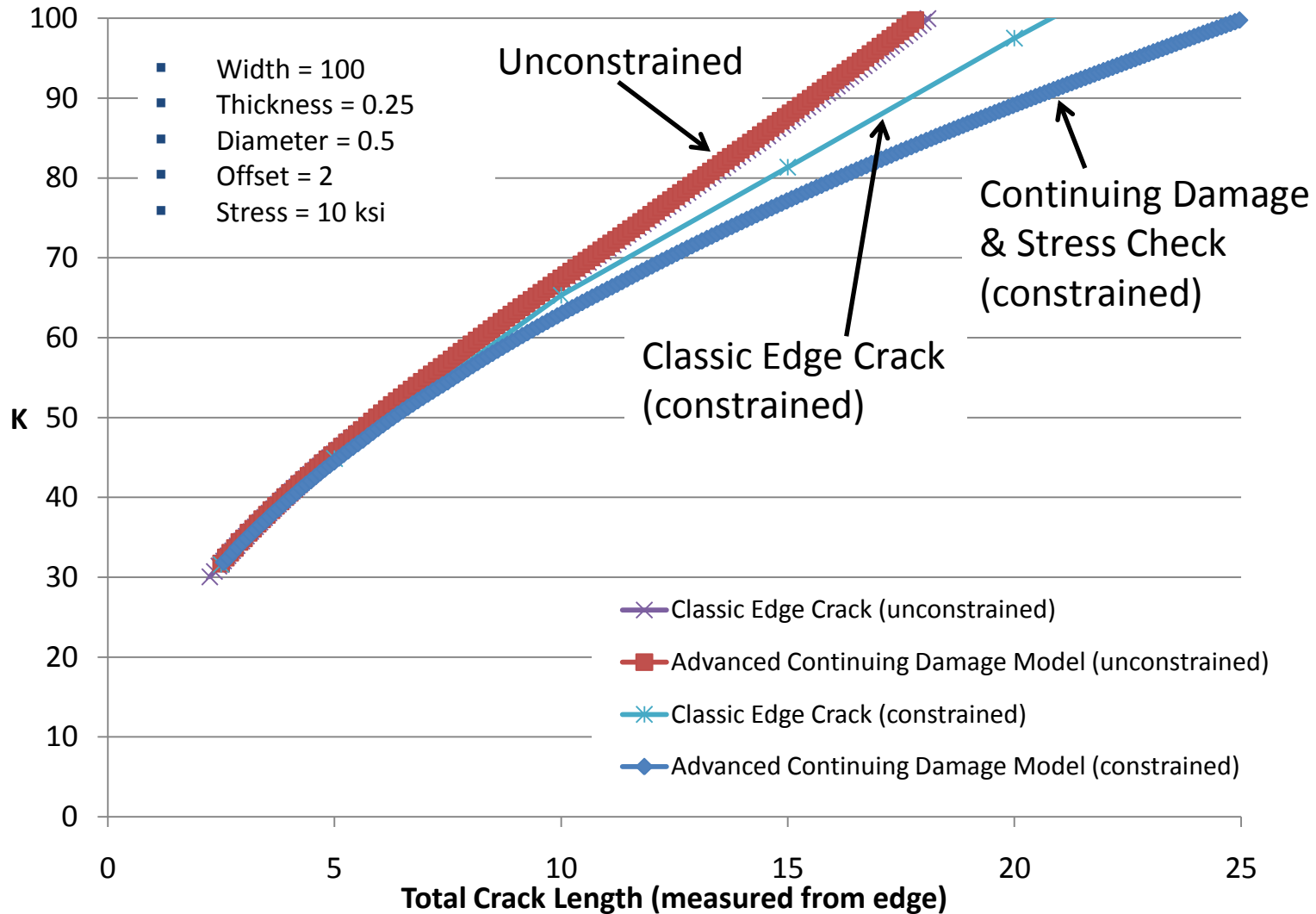




AFGROW Large Width Plate K Solutions



OGDEN AIR LOGISTICS CENTER

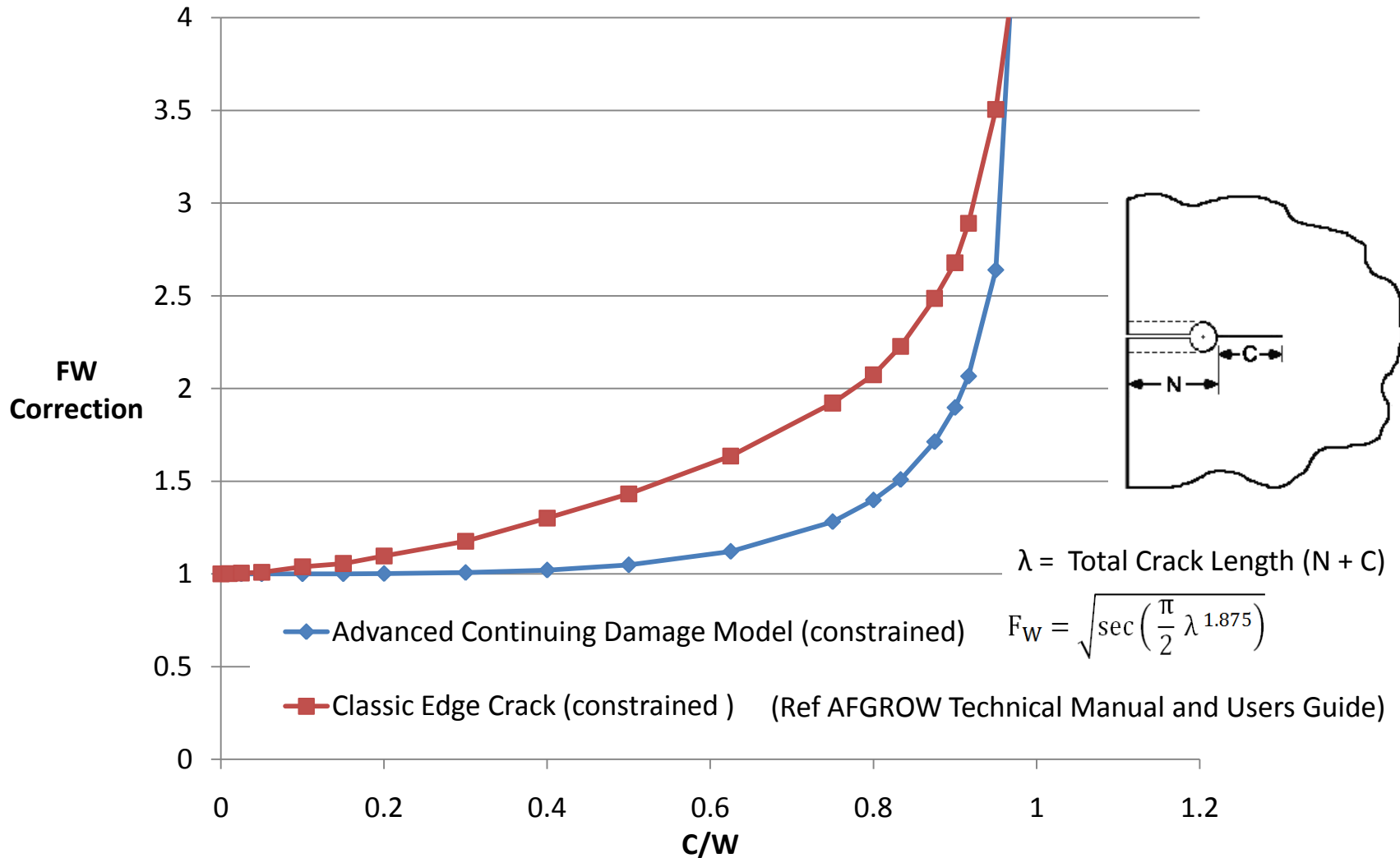




Finite Width Correction



OGDEN AIR LOGISTICS CENTER





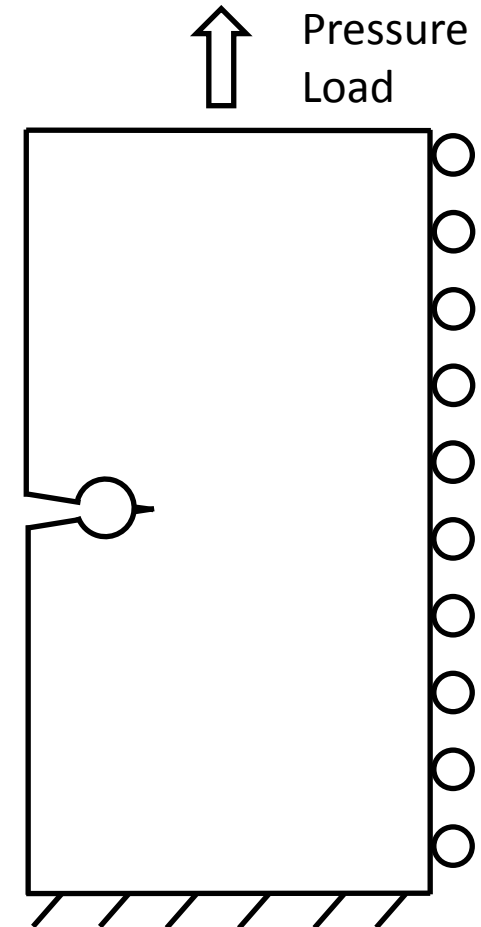
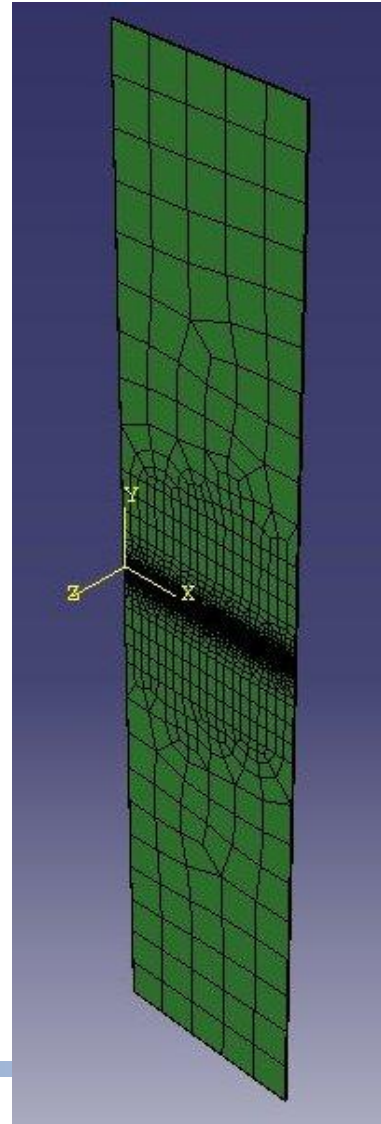
Continuing Damage FEM Constraints



OGDEN AIR LOGISTICS CENTER

- FEM:
 - ABAQUS w/FRANC3D/NG
- Dimensions
 - Width = $100 * N$
 - Thickness = 1
 - Total Height = $500 * N$
- Loading
 - Top Edge: Pressure Load
- Boundary Conditions:
 - Bottom Edge: Fixed in Y-Dir
 - Bottom Edge: Mid-Plane in Z-Dir
 - Right Edge: Fixed in X-Dir (Counteracts In-Plane Bending)

Ref: Harter, James A, AFRL/VASM,
2009



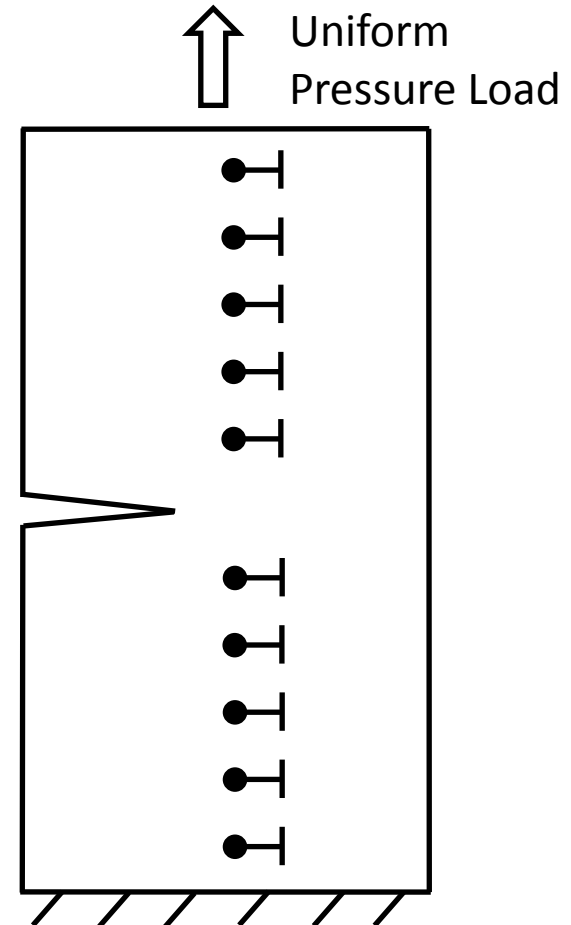


Classic Edge Crack FEM Constraints



OGDEN AIR LOGISTICS CENTER

- FEM:
 - FRANC2D
- Loading
 - Top Edge: Pressure Load
- Boundary Conditions:
 - Bottom Edge: Fixed in Y-Dir
 - Mid-Plane Nodes: Fixed in X-Dir
 - upper and lower portions of the plate only
 - Nodes in the area of the crack plane not constrained



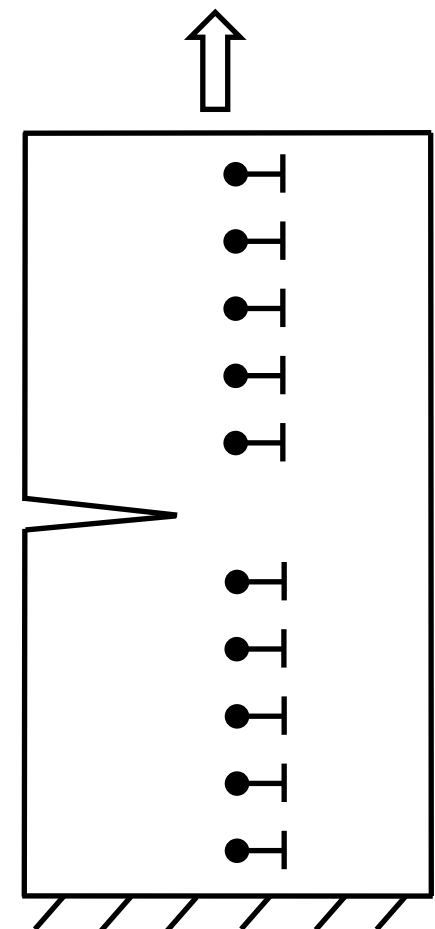
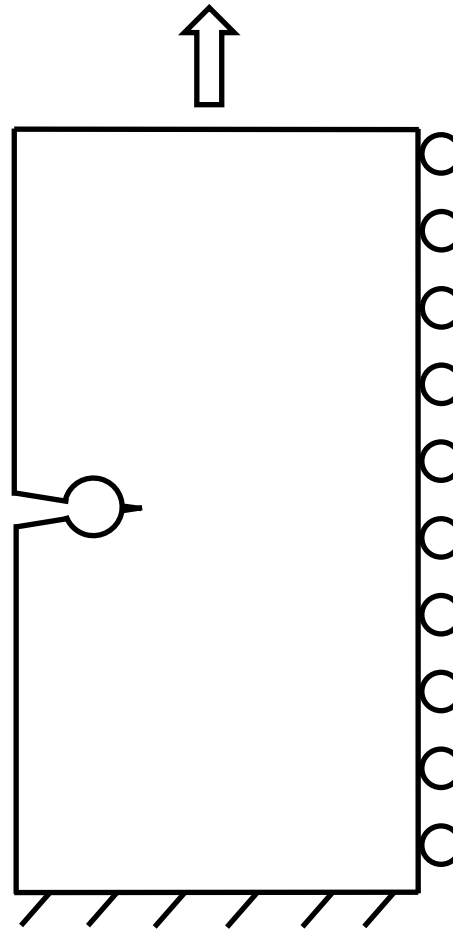


Appropriate Constraints?



OGDEN AIR LOGISTICS CENTER

- Comparison to Actual Structure
 - Fasteners constrain structure





Conclusions & Recommendations



OGDEN AIR LOGISTICS CENTER

- **Conclusions:**
 - Stress Intensity Solutions are significantly different when comparing Continuing Damage Model and Classic Edge Crack Model (In-Plane Bending Constrained)
 - Differences originate with FEM (constraints)
 - How much does it matter?
 - Continuing Damage Life (especially through crack) is typically small
 - Constraint assumption would also affect corner crack continuing damage life
 - Critical Crack Size
- **Recommendations:**
 - Replicate Edge Crack FEM and verify solutions
 - Investigate different constraint assumptions
 - Test data for a continuing damage case